Towards More Accurate and Efficient Integration of the UFS

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FV3 Time Stepping/Coupling

- Physics (Δt_{atmos})
- Tracer Transport and Vertical Remapping ($\Delta t_{atmos}/k_{split}$)
- Dynamics ($\Delta t_{atmos} / \{k_{split} * n_{split}\}$)



FV3 Stability Limits

- Horiztonal:
 - maximum stable $\Delta t_{dynamics} \sim \Delta x / (U + c_{acoustic})$
- Vertical: "No vertical CFL constraints"
 - A review by Griffies et al. 2020 (JAMES)
 - For the hydrostatic case:
 - "...there are no corresponding vertical CFL constraints for either tracer or velocity. Positive layer thicknesses are ensured for time-explicit methods if the horizontal (within layer) CFL constraint is maintained by the horizontal transport."
 - For the non-hydrostatic case:
 - "The key condition is that one must enable regridding at a <u>sufficiently fine time resolution</u> to maintain monotonic vertical grid layering and thus to prevent grid singularities."

Application/Description	Dynamics time step (actual)	Maximum Stable Dynamics time step (linear analytic)
HAFS_A	2.25 seconds	4.0 seconds
Finest grid 2.0 km	(Equates to	(Assumes max
k_split=4, n_split=10, dt_atmos=90 s, ptop=2 hPa	U+c = 889 m/s)	U+c = 500 m/s)
<u>HAFS_B</u>	2.50 seconds	4.0 seconds
Finest grid 2.0 km	(Equates to	(Assumes max
k_split=4, n_split=9, dt_atmos=90 s, ptop=2 hPa	U+c = 800 m/s)	U+c = 500 m/s)
<u>RRFS_A</u>	3.60 seconds	6 seconds
Finest grid 3.0 km	(Equates to	(Assumes max
k_split=2, n_split=5, dt_atmos=36 s, ptop=2 hPa	U+c = 833 m/s)	U+c = 500 m/s)
<u>RRFS_B</u>	3.33 seconds	6 seconds
Finest grid 3.0 km	(Equates to	(Assumes max
k_split=6, n_split=3, dt_atmos=60 s, ptop=2 hPa	U+c = 909 m/s)	U+c = 500 m/s)
GFS v15	18.75 seconds	22 seconds
Finest grid 13.0 km (C768)	(Equates to	(Assumes max
k_split=2, n_split=6, dt_atmos=225 s, ztop~55 km	U+c = 693 m/s)	U+c = 600 m/s)
<u>GFS v16</u>	12.50 seconds	22 seconds
Finest grid 13.0 km (C768)	(Equates to	(Assumes max
k_split=2, n_split=6, dt_atmos=150 s, ztop~80 km	U+c = 1040 m/s)	U+c = 600 m/s)

What's causing this inefficiency?

- Most cases work fine with the analytic time step size, but our operational systems need to be "bullet proof"
 - This requires an ~40% reduction in the acoustic time step size
 - For the GFS v16 application this equates to a potential ~25% reduction in atmospheric model efficiency
- Investigation has linked the crashes to non-monotonicity of LVC at the model top (we're violating the Lagrangian stability condition)
- Recent discussions with NASA (FV3-based GEOS model) appear to reveal this is a known issue associated with the vertical remapping method being used in the UFS
 Eurther investigation is required
 - Further investigation is required

How often should we perform vertical remapping?

- Most people I've talked to are fairly confused by the concept of the k_{split} variable; they
 don't really understand how often vertical remapping is necessary or why it's necessary
 - A review by Griffies et al. 2020 (JAMES)
 - For the non-hydrostatic case:
 - "The key condition is that one must enable regridding at a <u>sufficiently fine time resolution</u> to maintain monotonic vertical grid layering and thus to prevent grid singularities."
 - What is sufficient? How do we know a priori?
 - We don't know! We don't!
 - Why don't we just test for monotonicity/layer thickness on the fly to trigger remapping steps?

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Adaptive (in time) Remapping

- To start, set up time integrator as "while loop" instead of "for loop"
- Two options:
 - 1) Set a lower limit for layer thickness; if met, trigger a remapping step once the current dynamics step is finished (not guaranteed to finish the step)
 - 2) Store a copy of the state at the beginning of the dynamics step; if monotonicity is broken, replace the state, trigger a remapping step, and try again
- My hypothesis is that the necessary remapping frequency (for stability) is dependent upon a number of factors: grid resolution, terrain, flow characteristics, etc...it seems likely that for most relatively coarse resolution applications these issues are alleviated ($k_{split} \sim 1$)
 - Based on current UFS application values of k_{split} , this could save significant runtime

Physics-Dynamics Coupling

higher-order physics-dynamics coupling

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$$\frac{x^{n+1} - x^n}{\Delta t} \cong D + P$$

 The model attempts a tighter coupling between the dynamics and physics in which they are integrated together (in some fashion) to boost the global accuracy of the system beyond first order. first-order physics-dynamics coupling, aka, time splitting

$$\frac{\tilde{x} - x^n}{\Delta t} = D$$
$$\frac{x^{n+1} - \tilde{x}}{\Delta t} = P$$

 The physics and dynamics are performed separately ("black boxes") with minimal communication. The global system converges at first order.

Note that all fluxes from other components (ocean, land, ice, wave, etc) are or would be represented in the **P operator

"Dribbling" vs "Chunking"

Dribbling (proposed) coupling

- Physics (excluding microphysics) is run at the beginning of the time step (before dynamics); tendencies are stored
- Dynamics is integrated forward Δt_{atmos} . The physics tendencies are treated as static forcing terms on the RHS of the prognostic equations; they are applied at every "dynamics time step"
- After the dynamics the microphysics is called; the full microphysics tendencies are added to complete the time step
- The coupling frequency is >= the physics frequency
- GFS v16 coupling frequency would be 12.50 s

Chunking (control) coupling

- •
- Dynamics is integrated forward Δt_{atmos} ("physics time step") by way of several "dynamics time steps"
- The full physics package is called (with microphysics last)
- Physics tendencies are added as a single increment to complete the time step
- The physics and coupling frequencies are the same
- GFS v16 coupling frequency is 150 s



<group name="physics"> <subcycle loop="1"> <scheme>GF5_suite_interstitial_phys_reset</scheme> <scheme>GFS_suite_stateout_reset</scheme> <scheme>get prs fv3</scheme> <scheme>GFS suite interstitial l</scheme> <scheme>GFS surface generic pre</scheme> <scheme>GFS surface composites pre</scheme> <scheme>dcvc2t3</scheme> <scheme>GFS surface_composites_inter</scheme> <scheme>GFS suite interstitial 2</scheme> </subcycle> < --- Surface iteration loop --> <subcycle loop="2"> <scheme>mynnsfc wrapper</scheme> <scheme>GFS surface loop control partl</scheme> <scheme>lsm ruc</scheme> <scheme>flake driver</scheme> <scheme>GFS surface loop control part2</scheme> </subcycle> <!-- End of surface iteration loop --> <subcycle loop="1"> <scheme>GFS surface composites post</scheme> <scheme>sfc diag</scheme> <scheme>sfc diag post</scheme> <scheme>GFS surface generic post</scheme> <scheme>rrfs smoke wrapper</scheme> <scheme>mynnedmf wrapper</scheme> <scheme>rrfs smoke postpbl</scheme> <scheme>GFS GWD generic pre</scheme> <scheme>drag suite</scheme> <scheme>GFS_GWD_generic_post</scheme> <scheme>GFS suite stateout update</scheme> <scheme>ozphys 2015</scheme> <scheme>h2ophys</scheme> <scheme>get phi fv3</scheme> <scheme>GFS suite interstitial 3</scheme> <scheme>GFS suite interstitial 4</scheme> <scheme>GFS_MP_generic_pre</scheme> <scheme>mp thompson pre</scheme> <scheme>mp thompson</scheme> <scheme>mp thompson post</scheme> <scheme>GFS MP generic post</scheme> <scheme>maximum hourly diagnostics</scheme> <scheme>phys tend</scheme> </subcycle> </group>

<group name="microphysics"> <subcycle loop="1"> <scheme>GFS_suite_stateout_reset</scheme> <scheme>get prs fv3</scheme> <scheme>get phi fv3</scheme> <scheme>GFS suite interstitial 3</scheme> <scheme>GFS suite interstitial 4</scheme> <scheme>GFS MP generic pre</scheme> <scheme>mp thompson pre</scheme> <scheme>mp thompson</scheme> <scheme>mp thompson post</scheme> <scheme>GFS_MP_generic_post</scheme> <scheme>maximum hourly diagnostics</scheme> <scheme>phys tend</scheme> suite FV3 HRRR pdc </subcycle> </group> <group name="physics"> <subcycle loop="1"> <scheme>GFS_suite_interstitial_phys_reset</scheme> <scheme>GFS suite stateout reset</scheme> <scheme>get prs fv3</scheme> <scheme>GFS suite_interstitial_1</scheme> <scheme>GFS surface generic pre</scheme> <scheme>GFS surface composites pre</scheme> <scheme>dcyc2t3</scheme> <scheme>GFS_surface_composites_inter</scheme> <scheme>GFS suite interstitial 2</scheme> </subcycle> < --- Surface iteration loop --> <subcycle loop="2"> <scheme>mynnsfc_wrapper</scheme> <scheme>GFS surface loop control part1</scheme> <scheme>lsm ruc</scheme> <scheme>flake driver</scheme> <scheme>GFS_surface_loop_control_part2</scheme> </subcycle> < -- End of surface iteration loop --> <subcycle loop="1"> <scheme>GFS surface composites post</scheme> <scheme>sfc diag</scheme> <scheme>sfc diag post</scheme> <scheme>GFS_surface_generic_post</scheme> <scheme>rrfs smoke wrapper</scheme> <scheme>mynnedmf wrapper</scheme> <scheme>rrfs smoke postpbl</scheme> <scheme>GFS GWD generic pre</scheme> <scheme>drag suite</scheme> <scheme>GFS GWD generic post</scheme> <scheme>GFS suite stateout update</scheme> <scheme>ozphys 2015</scheme> <scheme>h2ophys</scheme> </subcycle> </group>

suite_FV3_HRRR

I've done my best to avoid modifying the code inside atmos_cubed_sphere, but obviously changes were necessary. From a user perspective you need to know 3 things:

- 1) When you compile, use {suite_FV3_HRRR, suite_FV3_HRRR_pdc}
- 2) Add higher_order_pdc = .true. to atmos_model_nml
- 3) Change ccpp_suite = 'FV3_HRRR_pdc'

```
&atmos_model_nml
    avg_max_length = 3600.
    blocksize = 32
    ccpp_suite = 'FV3_HRRR_pdc'
    chksum_debug = .false.
    dycore_only = .false.
    ignore_rst_cksum = .true.
    higher_order_pdc = .true.
```

Many of the changes live in the top level FV3 code, e.g., module_fcst_grid_comp.F90:

```
_____
! *** call fcst integration subroutines
    if (Atmos%higher order pdc) then
      call update atmos radiation physics (Atmos)
      call update atmos model tendencies (Atmos, rc=rc)
      if (ESMF LogFoundError(rcToCheck=rc, msg=ESMF LOGERR PASSTHRU, line=_LINE_, file=_FILE_)) return
      call update atmos model dynamics (Atmos)
      call update atmos microphysics (Atmos)
     else
      call update atmos model dynamics (Atmos)
      call update atmos radiation physics (Atmos)
     endif
     call atmos model exchange phase 1 (Atmos, rc=rc)
    if (ESMF LogFoundError(rcToCheck=rc, msg=ESMF LOGERR PASSTHRU, line= LINE , file= FILE )) return
    if (mype == 0) write(*, '(A, I16, A, F16.6)')'PASS: fcstRUN phase 1, n atmsteps = ', &
                                       n atmsteps,' time is ',mpi wtime()-tbegl
l _____
```

Some details of the "Dribbling" implementation in FV3 (latest iteration)

- I am working on a new iteration:
 - Inline_q = .false.
 - Apply tendencies in native dynamic variables (where possible)
 - Physics tendencies are held fixed in time and horizontal, they are advected as scalars in the vertical using Lagrangian advection (this looks like a mass re-scaling) such that we don't have to worry about boundary conditions.
 - The tendencies are applied on the C-grid and D-grid. This is done after the horizontal advection and requires further halo communication.
 - The tracer advection is in some ways decoupled from the dynamics across dt_atmos to prevent negatives and maintain conservation of dry mass
 - It was decoupled across k_split previously
 - The tracers will get the physics tendencies at the beginning of the time step ("chunking") and are still advected at k_split, but the tracer
 proxy variables (q_con, kappa) will evolve independently across dt_atmos. This is then resolved at the end of the time step by computing
 new proxy values using the fully updated tracers; they are then used to convert theta_m to temperature prior to physics.
- Potential Deficiencies:
 - Cost: hopefully < 10% added cost
 - My results say vertical interpolation vs vertical advection of physics tendencies is not significantly different, but I'd like some outside opinions on this
 - How different are the proxy variables by the end of a time step? Have we traded a physics coupling problem for a tracer coupling problem?

Conclusions

- It appears possible that we may be able to achieve greater stability, efficiency, and accuracy in the UFS with these three changes to the atmospheric model
 - Efficiency gains >25% may be possible, depending on the dynamics cost in the application
 - Could have implications for increasing ensemble sizes or decreasing computational resources
 - Accuracy gains from "dribbling" should increase with increasing Δt_{atmos} , which also depends on application (largest for GFS and S2S). However, unless the coupling is prohibitively expensive or intractable, I don't see a good reason to leave accuracy on the table